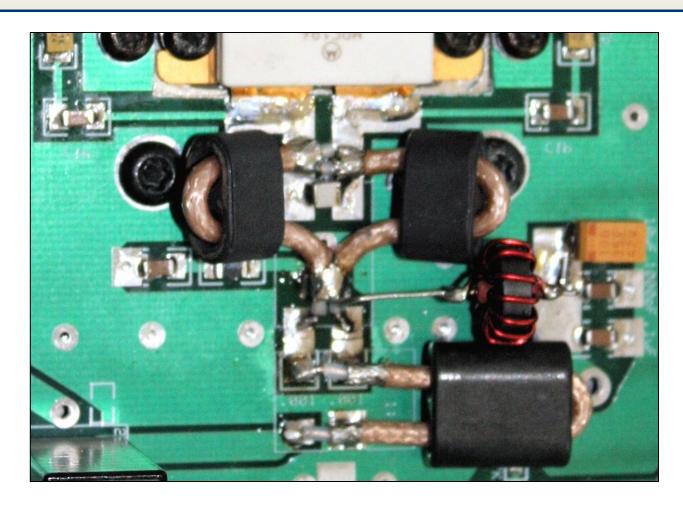
## **Transmission-Line Transformers**





### **Categories of Transmission-Line Transformers**

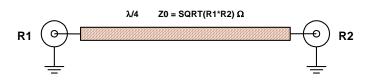
• Single  $\lambda/4$  lines and cascades of  $\lambda/4$  lines

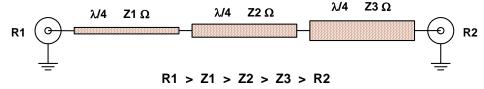
 Distributed element approximations of lumped element (LC) designs

- Short, highly coupled unit element structures
  - Ruthroff
  - Guanella

# $\frac{1}{4}\lambda$ and Stepped $\frac{1}{4}\lambda$ Transformers

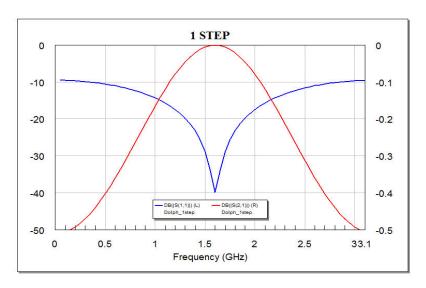
- Half octave performance from single quarter-wave line transformer
- Nearly 2-octave performance from 3 stepped quarter-wave lines
- Comparison for  $50\Omega$  to  $100\Omega$  transformation (BW also depends on this)

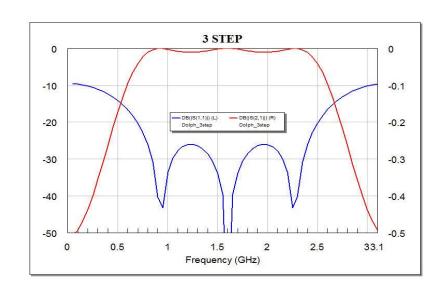




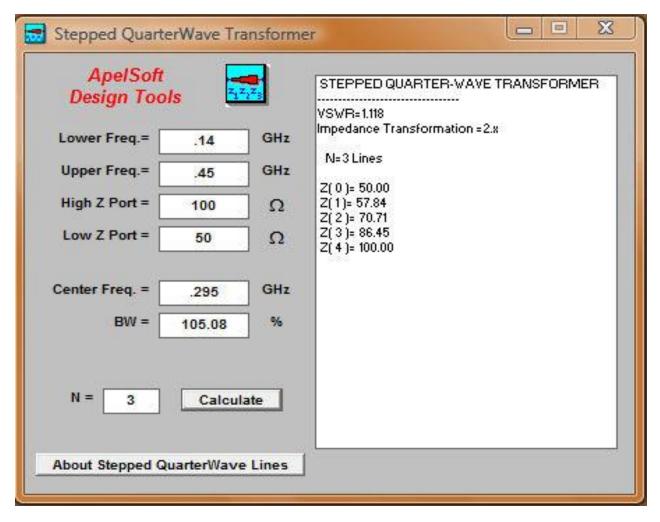
 $\frac{1}{4}\lambda$  7 INVERTER

STEPPED Z TRANSFORMER



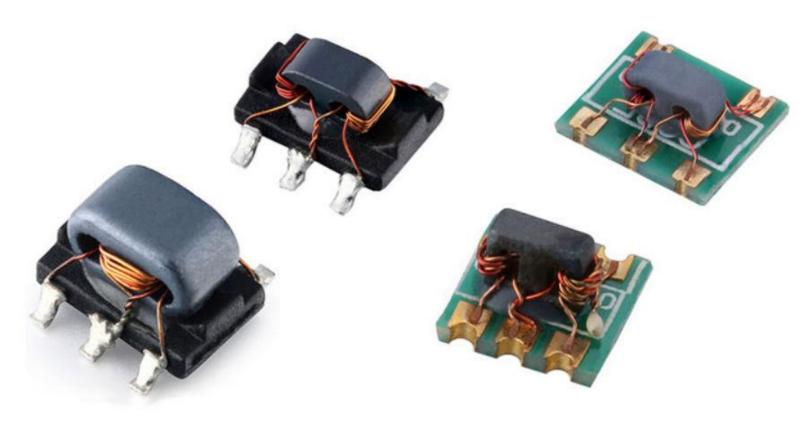


# Stepped ¼ \(\lambda\) Transformer Calculation



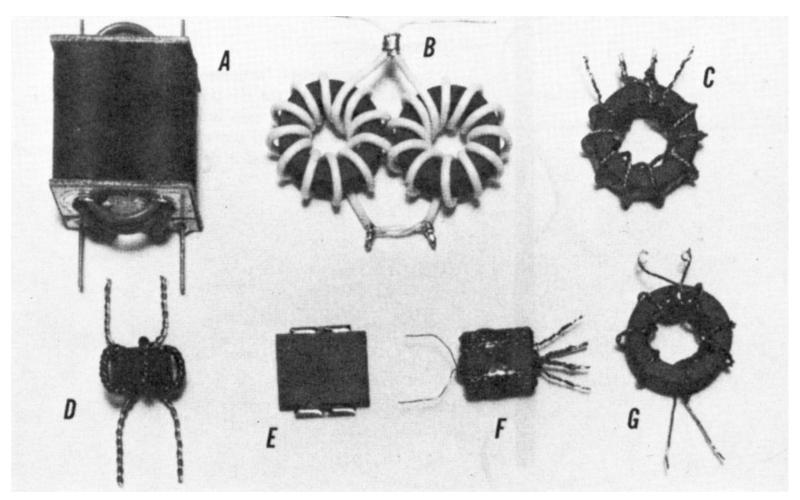
DOWNLOAD FROM: <a href="http://k5tra.net/">http://k5tra.net/</a>

#### Ferrite Loaded Transmission-Line Transformers



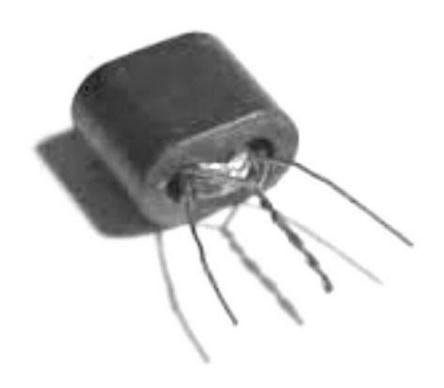
TWO HOLE BINOCULAR CORES and BIFILAR PAIRS

#### Ferrite Loaded Transmission-Line Transformers



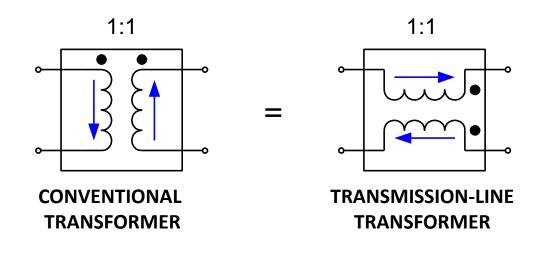
TWO HOLE BINOCULAR and TOROID CORES LINES FROM COAX, BIFILAR and TRIFILAR WIRES

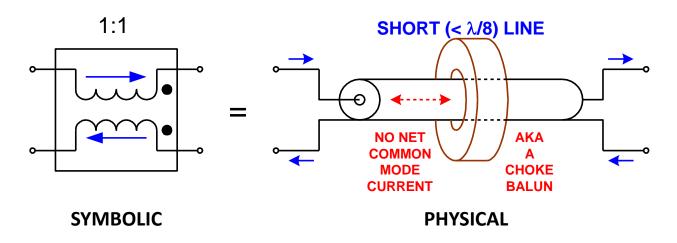
#### Ferrite Loaded Transmission-Line Transformers



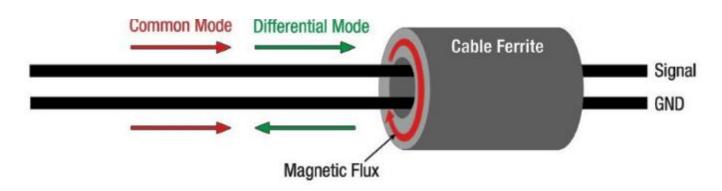
A RUTHROFF 4:1 TRANSFORMER USING BIFILAR TWISTED PAIR

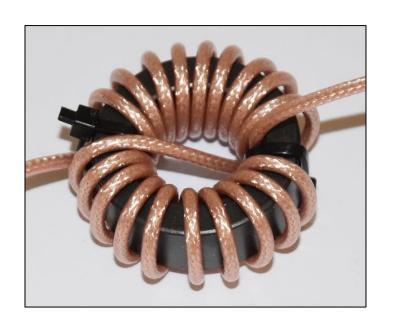
#### Transmission-Line Transformer – Elements





#### Ferrite-Loaded Transmission-Lines are Choke Baluns



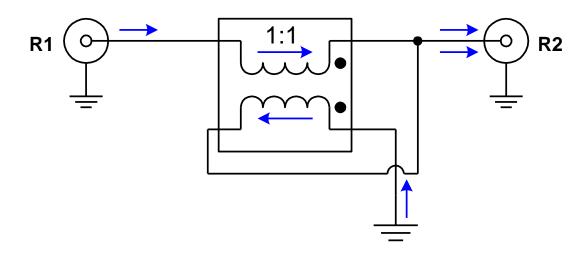


FERRITE
LOADING
PREVENTS
COMMON
MODE
CURRENT
FROM
FLOWING



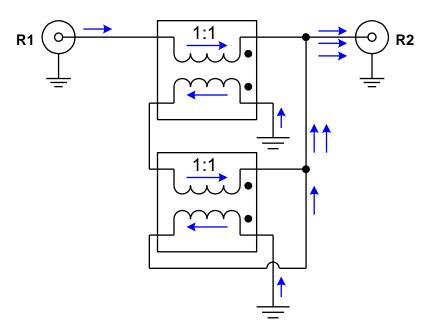
#### **Ruthroff Transformers**

- Transmission line 'unit' element
- Physically short lines (length  $< \lambda / 8$ )
- Analysis based on currents
- $R_1 / R_2 = (I_2 / I_1)^2 = 4$
- Ferrite loading extends bandwidth (low end)



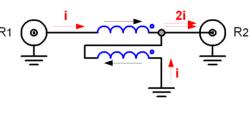
# Ruthroff Type 9:1 Transformer

- Transmission line 'unit' elements
- Physically short lines (length  $< \lambda / 8$ )
- Analysis based on currents
- $R_1 / R_2 = (I_2 / I_1)^2 = 9$
- Ferrite loading extends bandwidth (low end)



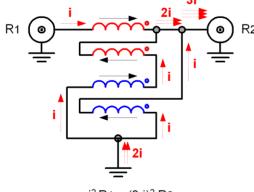
### Various Unbalanced Transformers

- Transmission line unit element building blocks
- Parasitic even mode characteristic impedance should be large (k → 1)
- Z ratio available as squares of integer ratios
- First order analysis on basis of port current ratio
- Multiple line structures must have at least one shared current path
- DC path is present



 $i^2 R1 = (2 i)^2 R2$ R1 = 4 R2

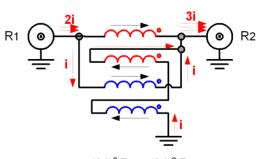
4:1 Transformer



 $i^2 R1 = (3 i)^2 R2$ 

R1 = 9 R2

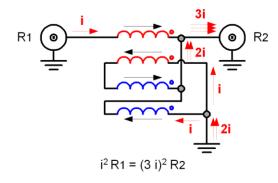
9:1 Transformer version - A



 $(2 i)^2 R1 = (3 i)^2 R2$ 

R1 = 4 R2

4:9 Transformer (approx. 1:2)

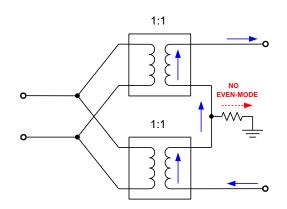


9:1 Transformer version - B

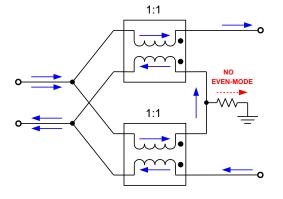
R1 = 9 R2

## Guanella (4:1) Balanced Transformer

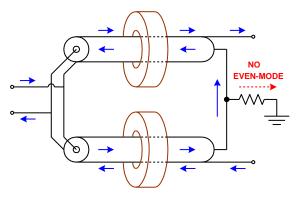
- Two 'unit' elements can be used to form a balanced 4:1 transformer
- Analysis based on currents
- $R_1 / R_2 = (I_2 / I_1)^2 = 4$
- Ferrite loading extends bandwidth (low end)



CONVENTIONAL 4:1 BALANCED TRANSFORMER



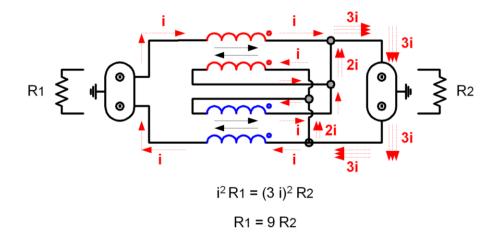
GUANELLA 4:1
SYMBOLIC



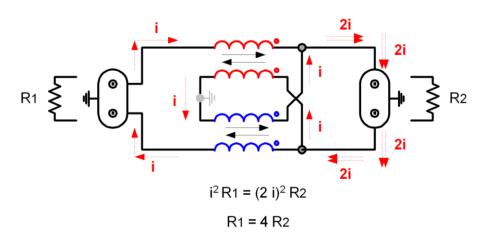
GUANELLA 4:1
PHYSICAL

#### Several Balanced Transformers

- Transmission line unit element building blocks
- Parasitic even mode characteristic impedance should be large (k → 1)
- Z ratio available as squares of integer ratios
- First order analysis on basis of port current ratio
- Multiple line structures must have at least one shared current path
- DC path is present



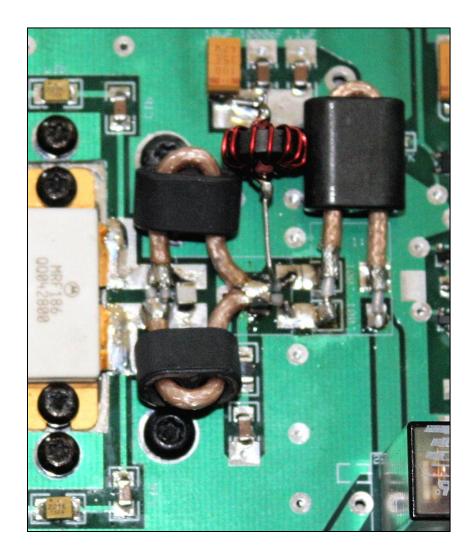
9:1 Transformer



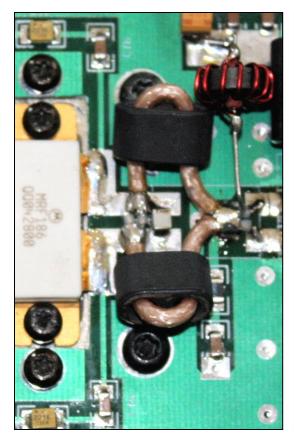
4:1 Transformer

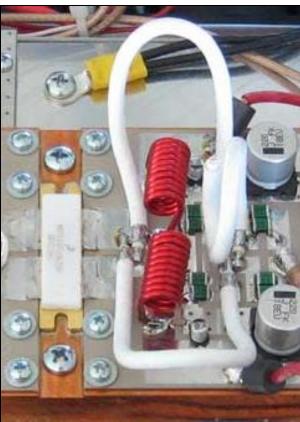
#### Guanella Transformer and Choke Balun

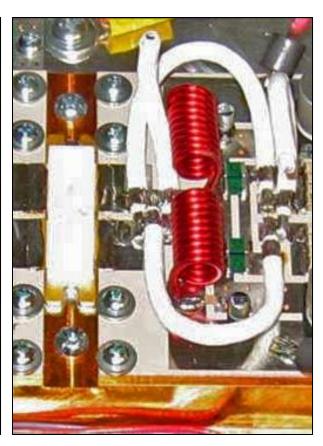
- Pushpull PA match example
- Ferrite loaded 'unit' elements
- Guanella transformer from coax
- Choke balun (1:1) from coax



## More Guanella Transformers in PA Output







- Guanella transformer from coax
- 'Unit' elements with and without ferrite loading

# Coupled Lines - Symmetric

- Two transmission-line modes
  - Even (or common) mode
  - Odd (or differential) mode
- Impedances set coupling level

DIELECTRIC

METAL

METAL

METAL

# **Coupling Coefficient**

$$Zoe/Zoo = (C+2CM)/C$$

$$k = \frac{Zoe/Zoo - 1}{Zoe/Zoo + 1}$$

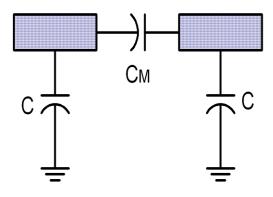
$$k = \frac{CM}{CM + C}$$

$$k = \frac{CM}{CM + C} = \frac{\frac{CM}{C}}{\frac{CM}{C} + 1}$$

$$Zoe/Zoo \rightarrow \infty \Rightarrow K\rightarrow 1$$

$$C_M/C \rightarrow \infty \Rightarrow K \rightarrow 1$$

- Zoo sets the desired Zo
- Zoe should be large!



STATIC CAPACITANCE REPRESENTATION FOR SYMMETRIC STRUCTURES

# Coupled Lines - Asymmetric

- Asymemetric coupled lines
  - Two modes: C and  $\pi$
  - Similar to 'Even' and 'Odd'
- Impedances set coupling level

DIELECTRIC METAL

METAL

METAL

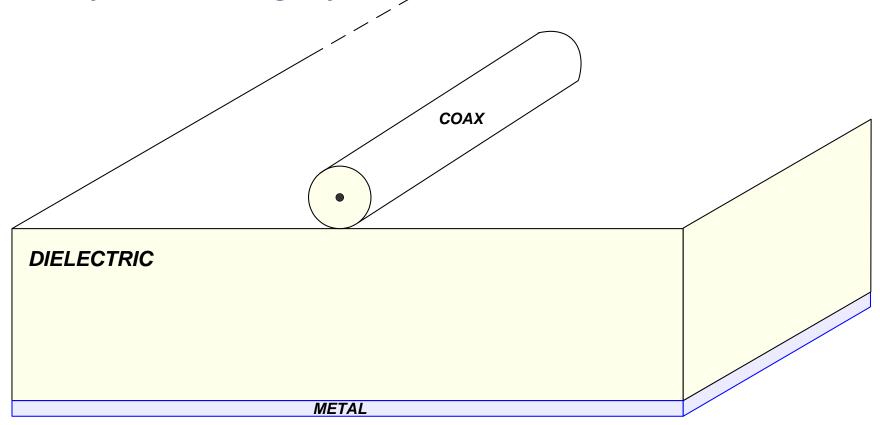
# Coupled Lines - Asymmetric

• Broadside coupling is better

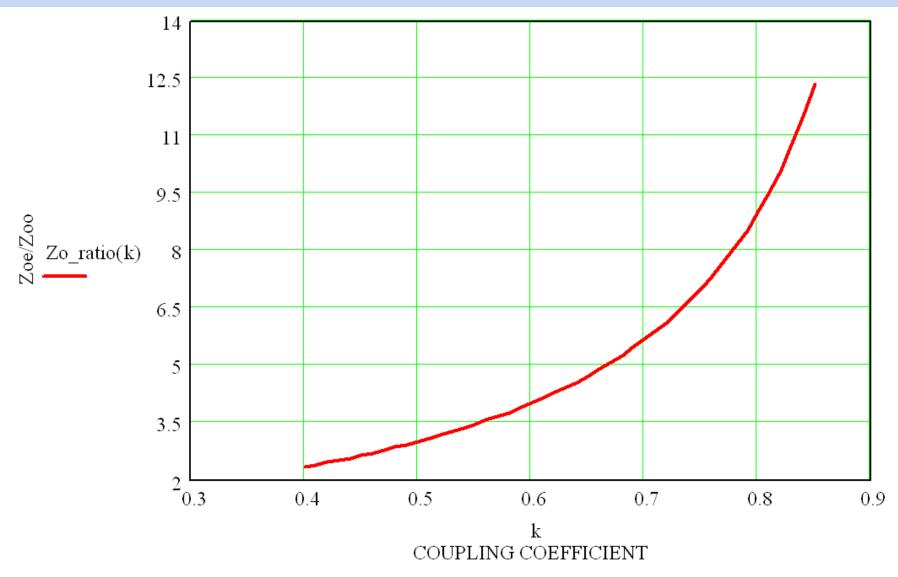
• Asymmetric: slightly unbalanced METAL METAL **DIELECTRIC** METAL

## Coax Over Ground

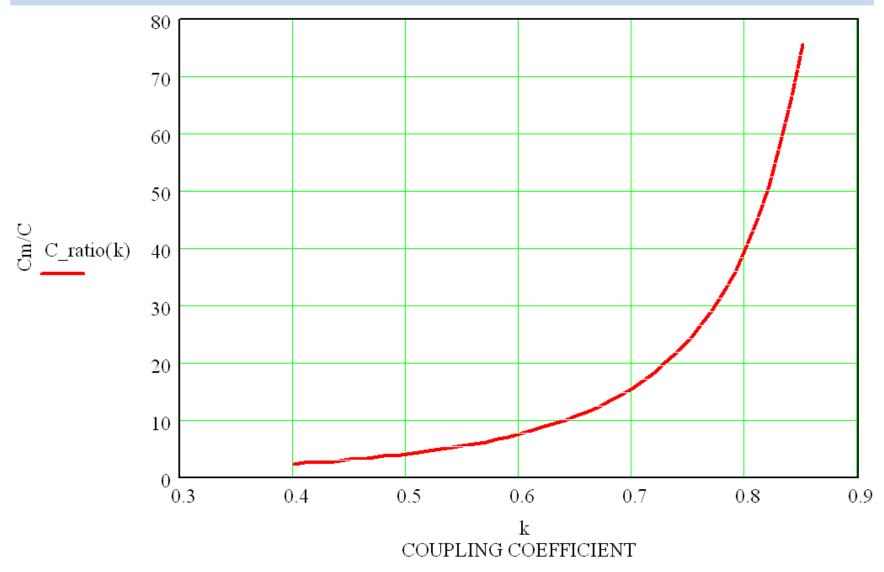
- Coax coupling is very good
- Asymmetric: slightly unbalanced



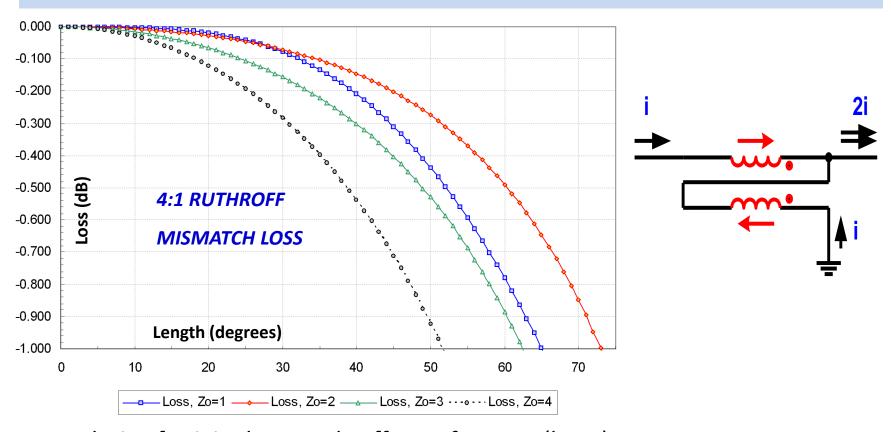
# Coupling Coefficient Relationship to Zoe/Zoo



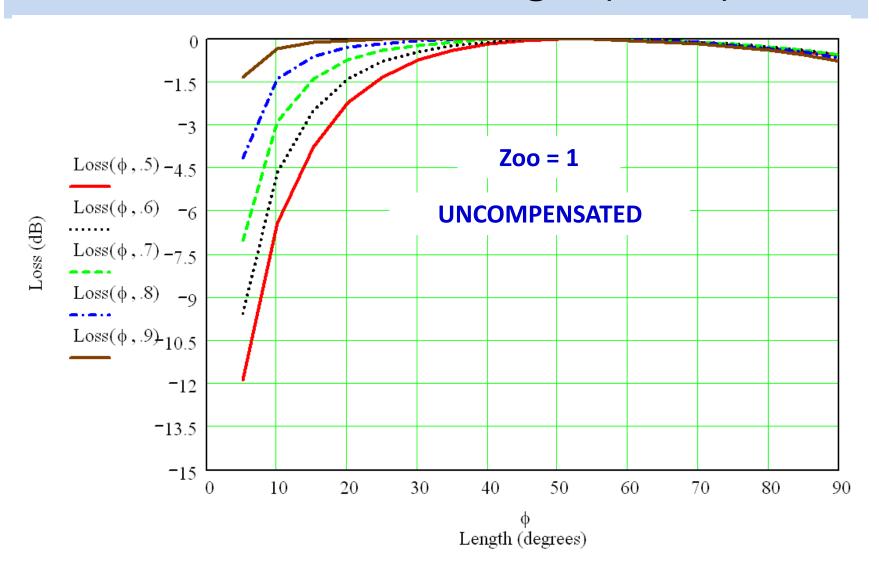
# Coupling Coefficient Relationship to C<sub>m</sub>/C

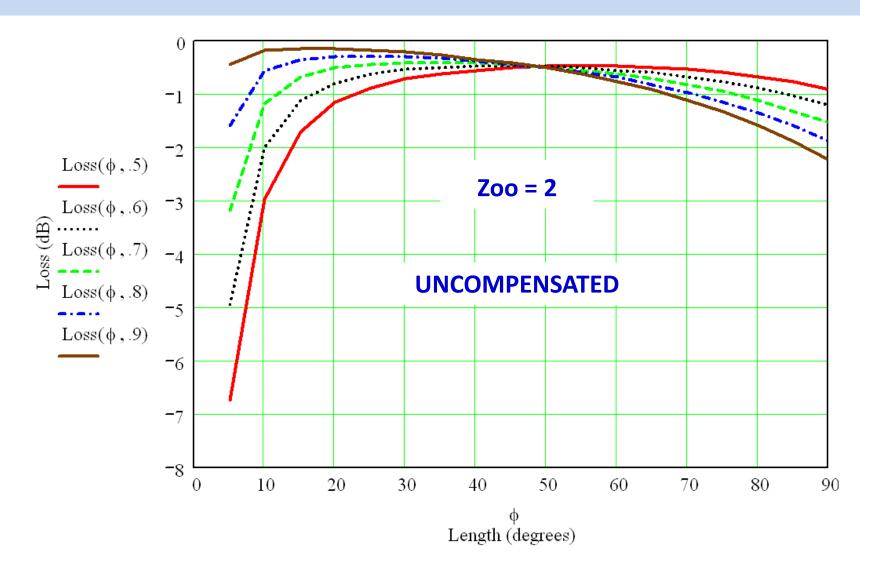


# Ideal Ruthroff Loss vs Length (and Zo)

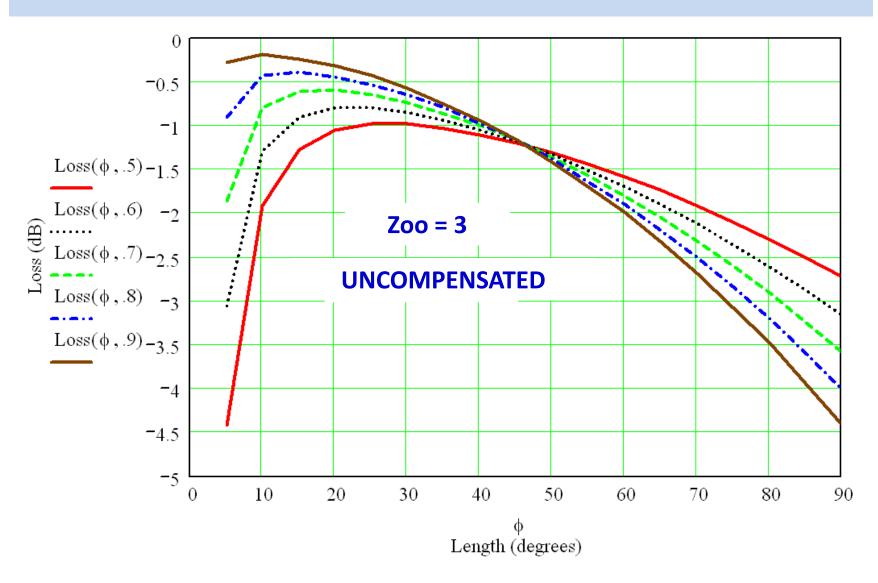


- Analysis of original 4:1 Ruthroff transformer (k = 1)
- Normalized port impedances (1 $\Omega$  and 4 $\Omega$ )
- Best BW from Zo=2
- Lowest loss over less BW from Zo=1





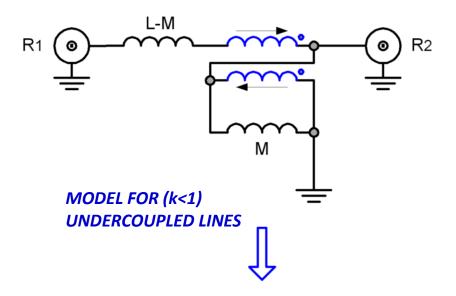


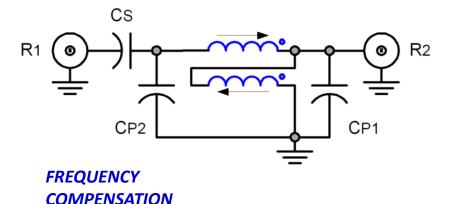


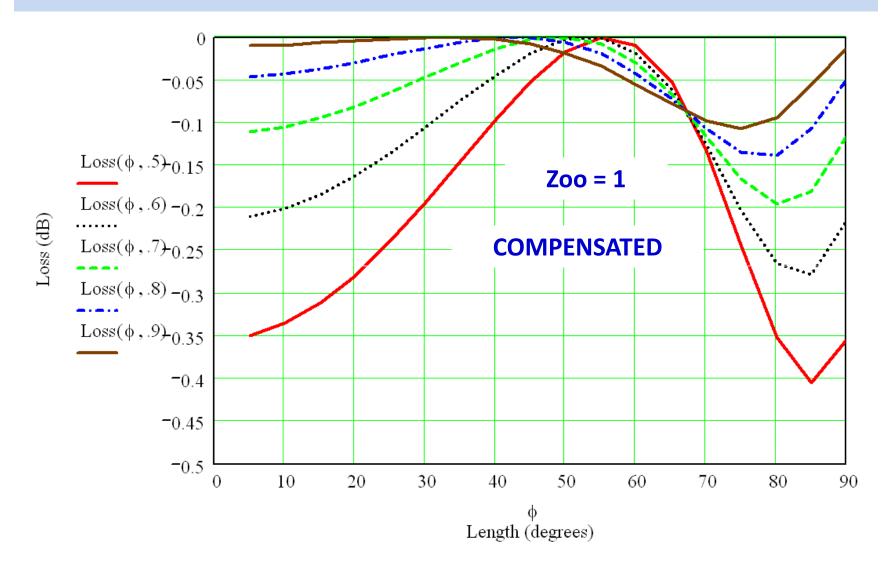


### Ruthroff Transformer Frequency Compensation

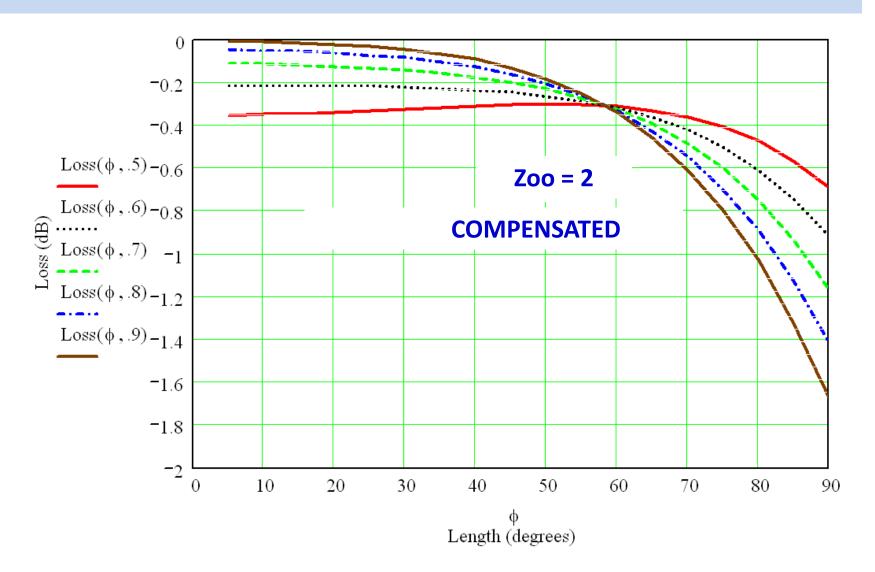
- Non-ideal coupling is modeled by leakage and magnetizing inductance
- Cs provides DC block and low frequency compensation
- CP1 and CP2 provide high frequency compensation
- If coupling is poor, or Zoo is not optimal, Cp can be used to tune the transformer for the desired frequency band



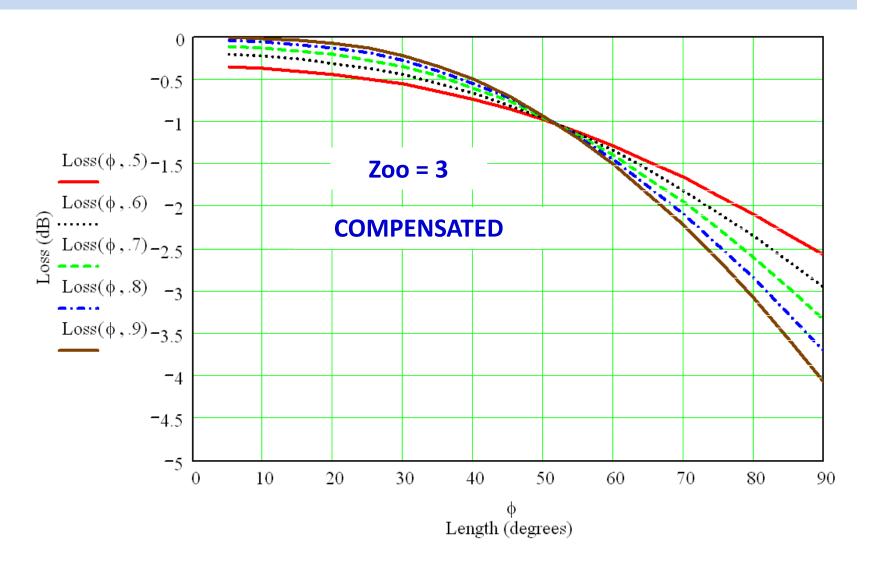






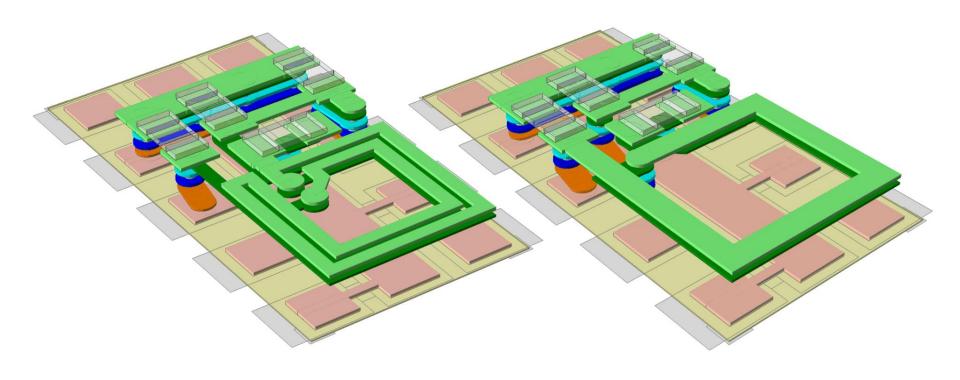








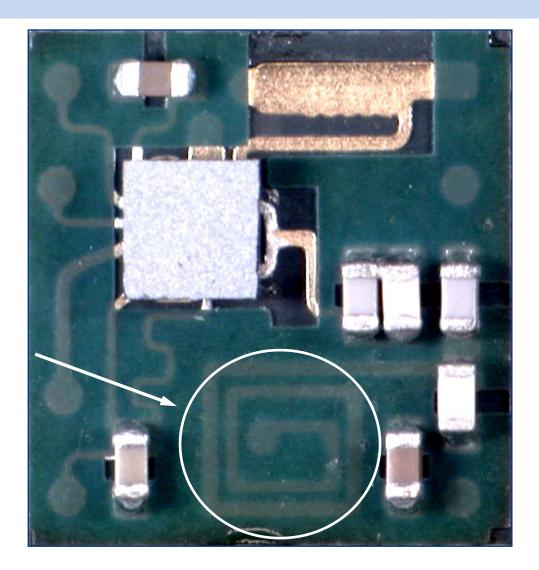
### Ruthroff Transformer Test Laminates



9:1 TRANSFORMER

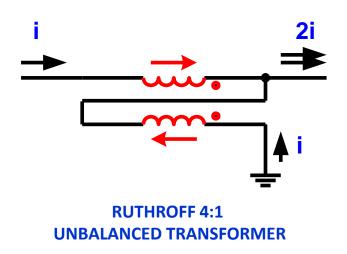
**4:1 TRANSFORMER** 

# Flip Chip Multiband PA with Ruthroff 4:1

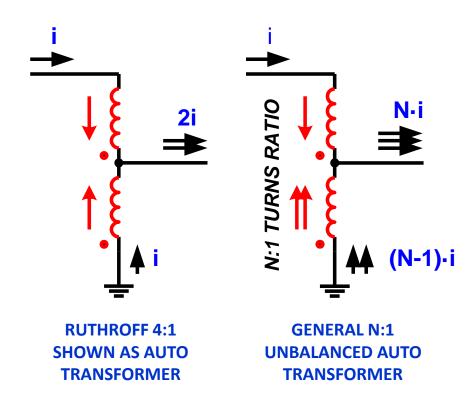


RUTHROFF 4:1
TRANSFORMER

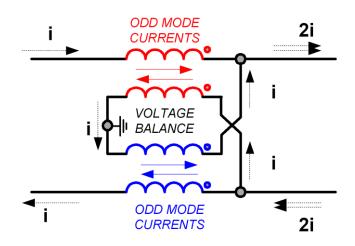
### Ruthroff Relationship to Auto Transformers



- The Ruthroff structure can be redrawn as an auto transformer special case (N=2).
- Transformation can be set by setting the tap (1/N is tapped fraction of total primary)

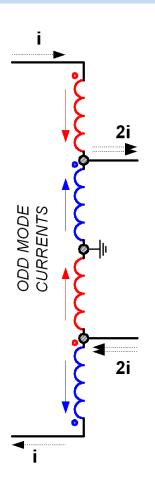


### Guanella Relationship to Auto Transformers

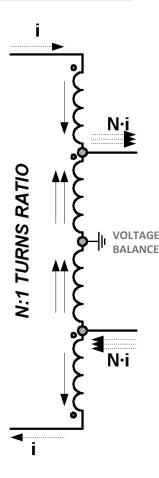


GUANELLA 4:1 BALANCED TRANSFORMER (BALBAL)

- The Guanella balanced structure can be redrawn as an auto transformer special case (N=2). - note couplings –
- A more general auto transformer has secondary coupled to both primary segments
- Transformation can be set by setting the taps (1/N is tapped fraction of total primary)

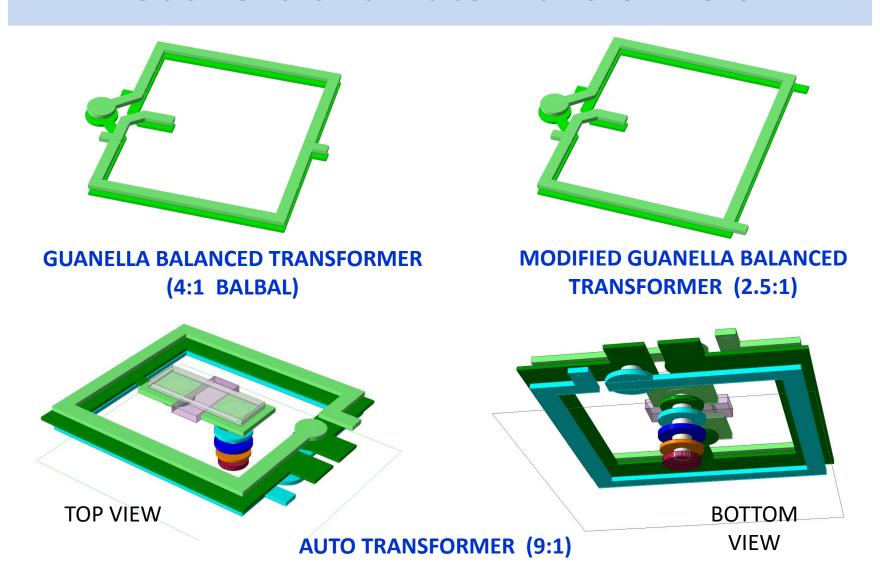




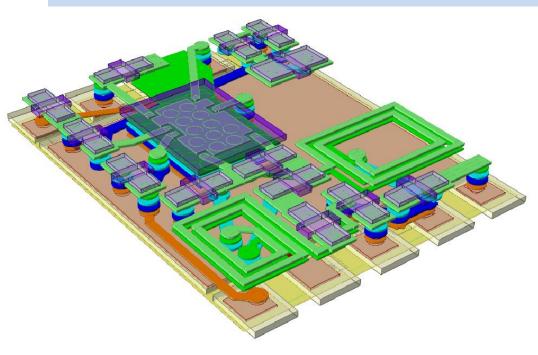


GENERAL N:1
BALANCED AUTO
TRANSFORMER

## **Guanella and Auto Transformers**

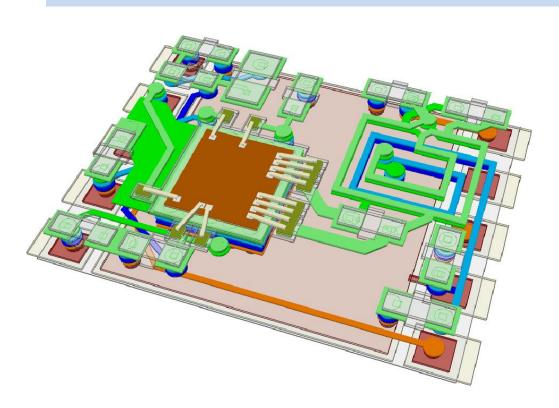


# Wideband Flip Chip PA Module

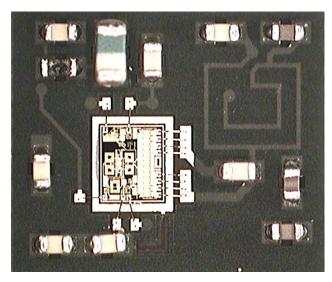


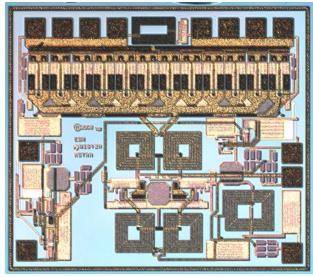
- 800 MHz 2 GHz
- WCDMA operation

### Pushpull Multimode PA

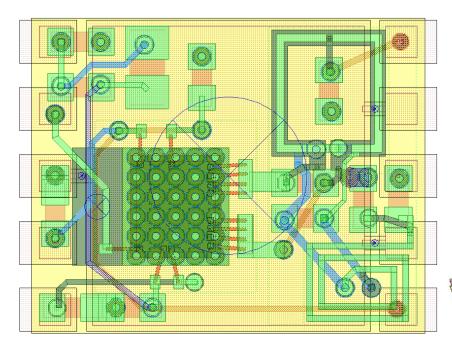


- Laminate contains modified Guanella transformer stacked with choke balun
- Full 824 915 MHz operation
- WCDMA, EDGE, and GSM



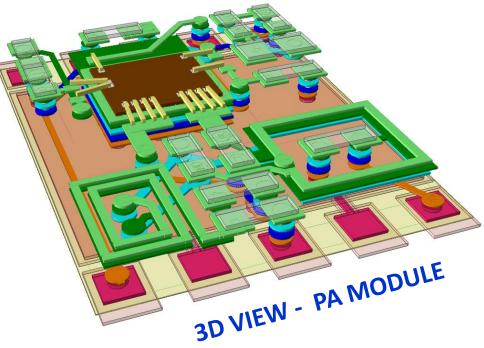


## Low V Pushpull Multimode PA

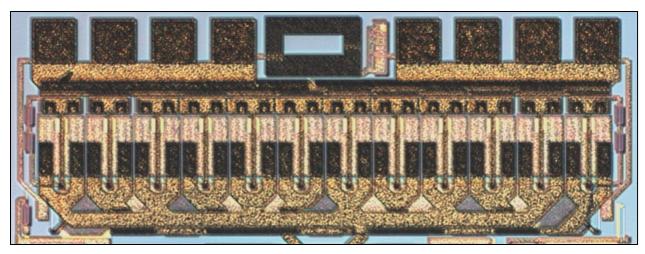


5mm x 4mm PA MODULE (.20" x .16")

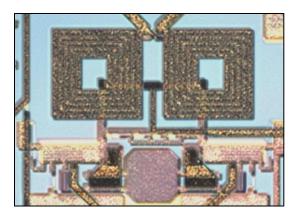
- Low Vcc operation provided by high ratio transformer
- Three metal layers are used in a 9:1 auto-transformer
- Choke balun



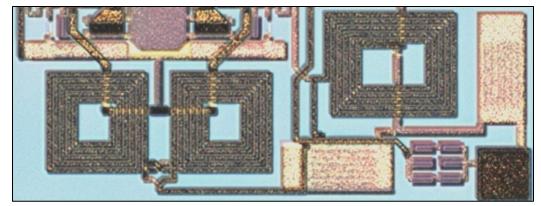
# GaAs Pushpull PA Circuit Blocks



ARRAY OF OUTPUT CELLS WITH INTERLEAVED MANIFOLD AND 3<sup>RD</sup> HARMONIC TUNING



INTERSTAGE GUANELLA TRANSFORMER



INPUT CHOKE BALUN and GUANELLA TRANSFORMER

# Summary

- Transmission-line transformers
  - 3 categories
- Coupled lines
  - Coupling coefficient
  - Capacitive compensation
- Unbalanced or balanced forms

Ruthroff: unbalanced

- Guanella: balanced

- Autotransformers
- Some examples

